

REINHOLD ENVIRONMENTAL Ltd.



2011 NO_x-Combustion Round Table & Expo Presentation

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Gas-Gas Mixing Fundamentals for SCR

*NO_x - Combustion Round Table & Expo
Birmingham, 2011*

Kevin Rogers
Advisory Engineer

Gas-Gas Mixing Fundamentals for SCR

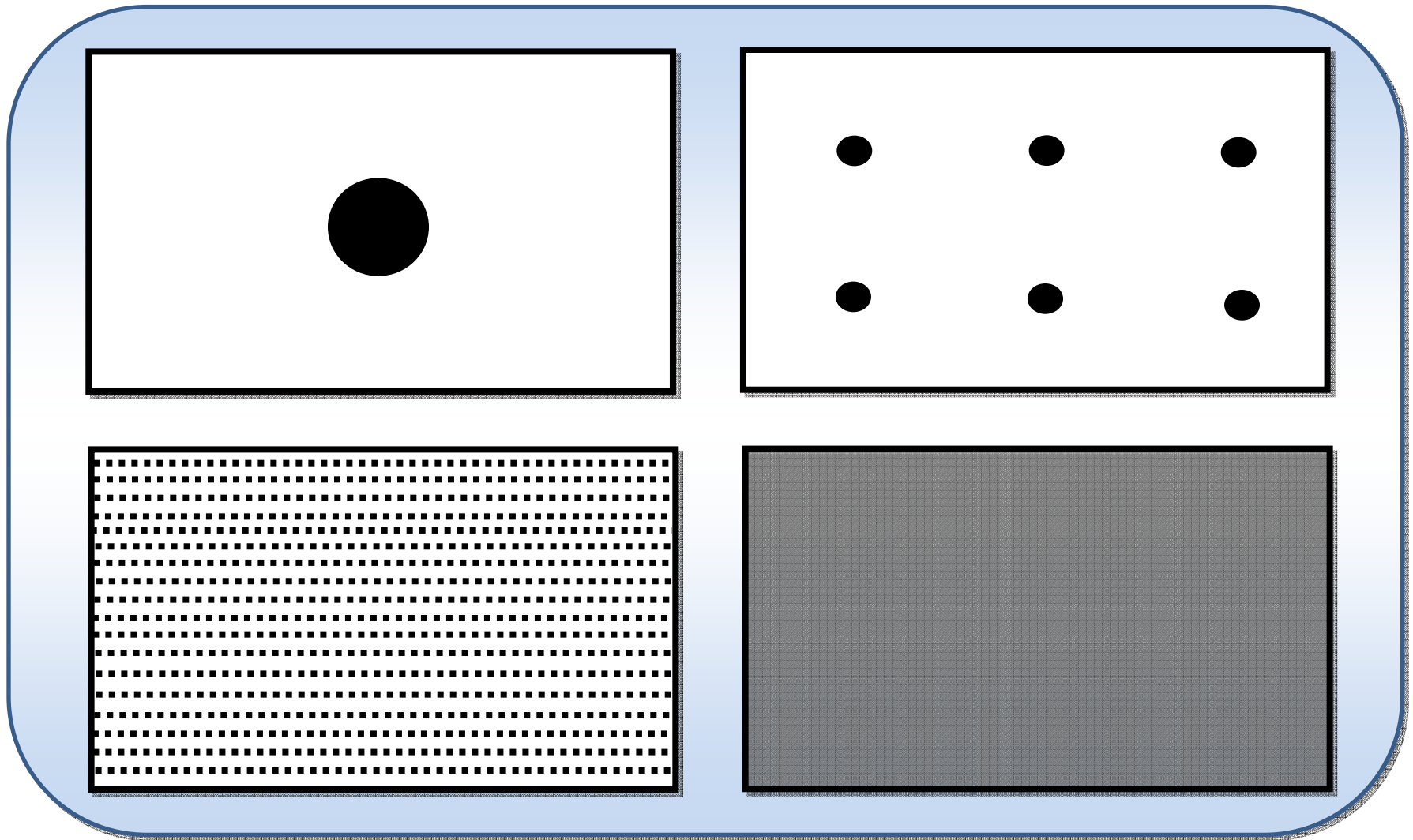
Topics

- ▶ ***Introduction***
- ▶ ***Basic Mixing Theory***
- ▶ ***Types of Mixers & Mixing Approaches***
- ▶ ***Performance Analysis for Development***
 - Effectiveness
 - Efficiency
- ▶ ***Ammonia Injection***
- ▶ ***Field Results***
- ▶ ***Summary***

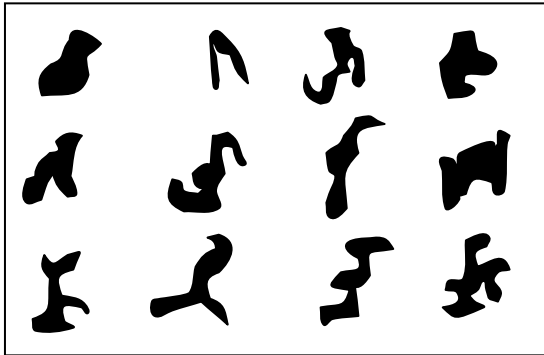
Mixing – Science & Art

- ▶ ***Art*** - Combining the science and the application in the best, most effective manner
- ▶ ***Science (Old & New)*** - Then (1940-1960) versus now (2011)
- ▶ ***Similarities across disciplines*** - Mixing of liquid-liquid, liquid-solids, liquid-gases, liquid-gases-solids, solids-solids, gases-solids, gases-gases. Many parallels in dosing, blending function, and residence time distributions
- ▶ ***Three basic degrees of freedom***
 - Process result
 - Time or distance
 - Energy

Scale of Segregation



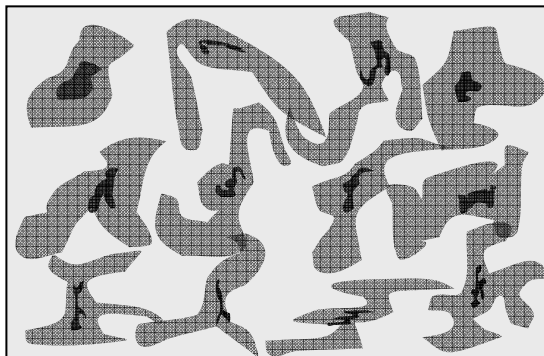
Scale and Intensity of Segregation



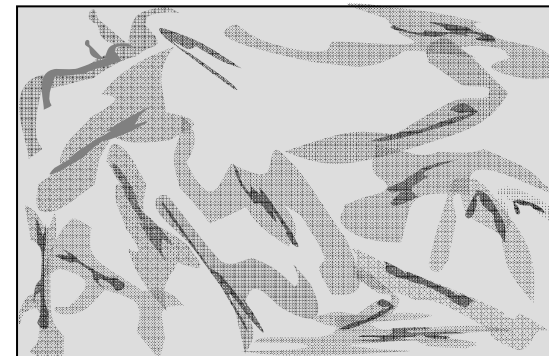
Decreasing
Scale of
Segregation
→



Decreasing
Intensity of
Segregation
↓



Decreasing
Intensity of
Segregation
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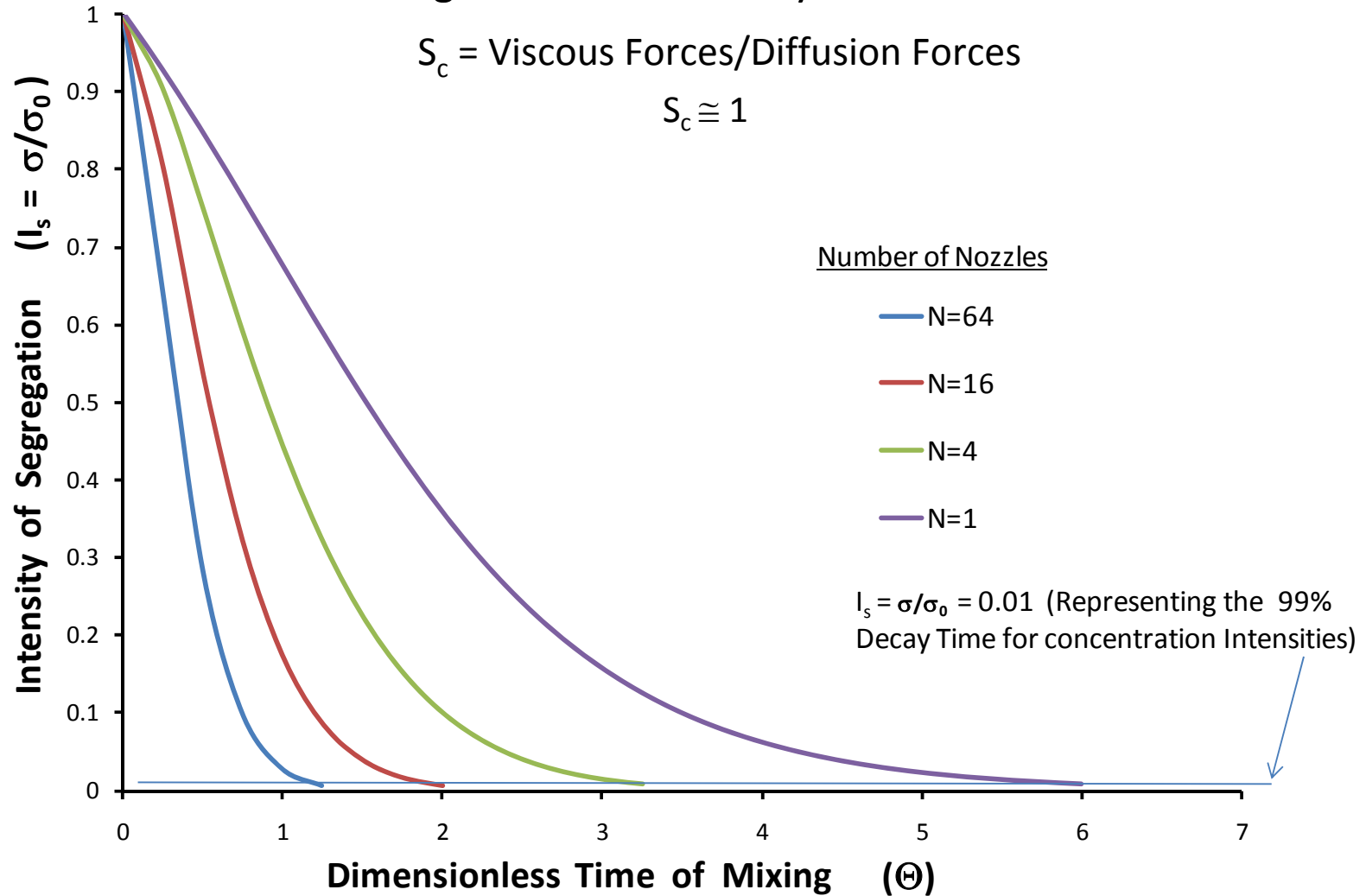


Turbulent Mixing Theory

Gas-Gas Mixing – Characterized by low Schmidt Numbers

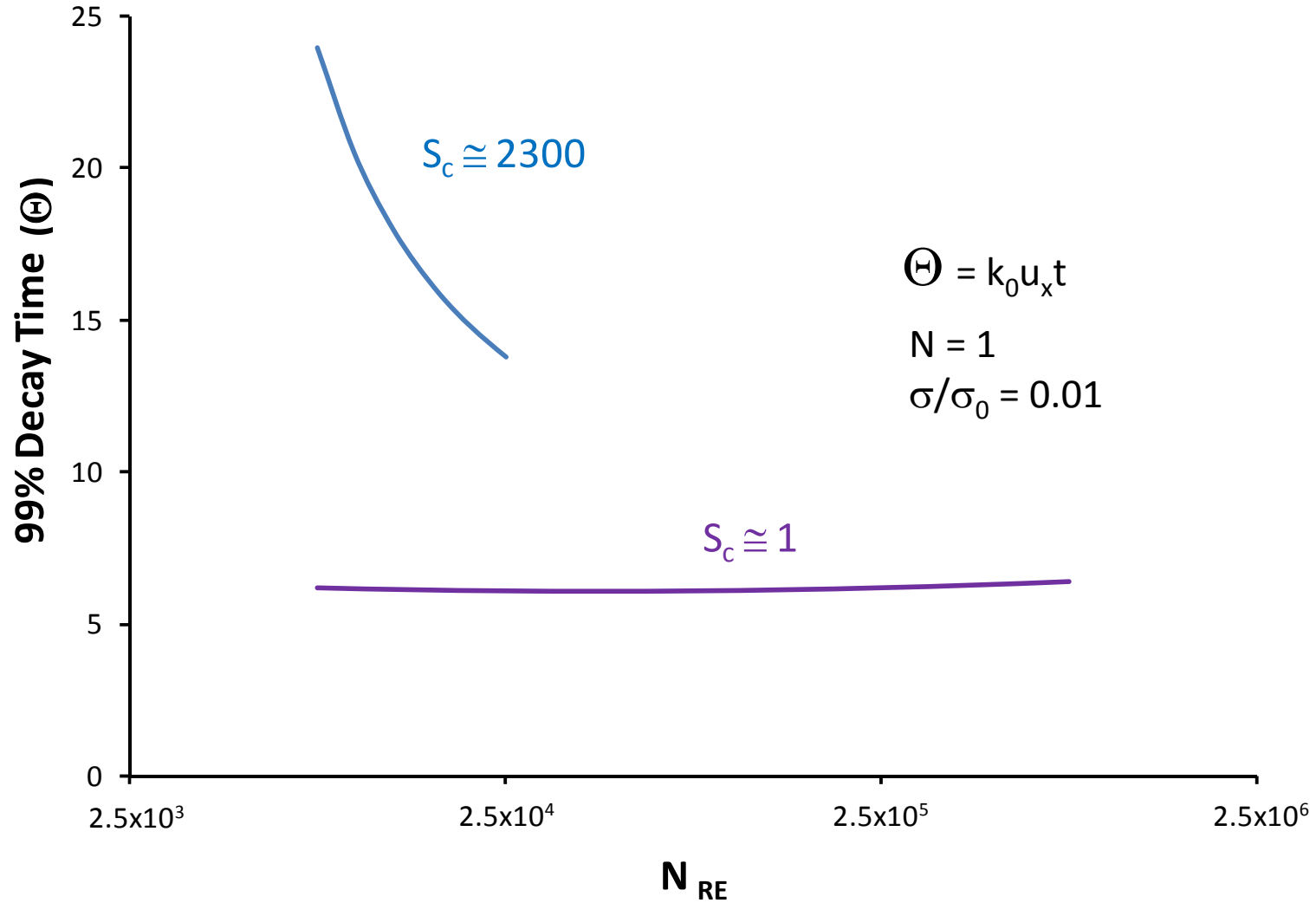
$S_c = \text{Viscous Forces/Diffusion Forces}$

$$S_c \cong 1$$

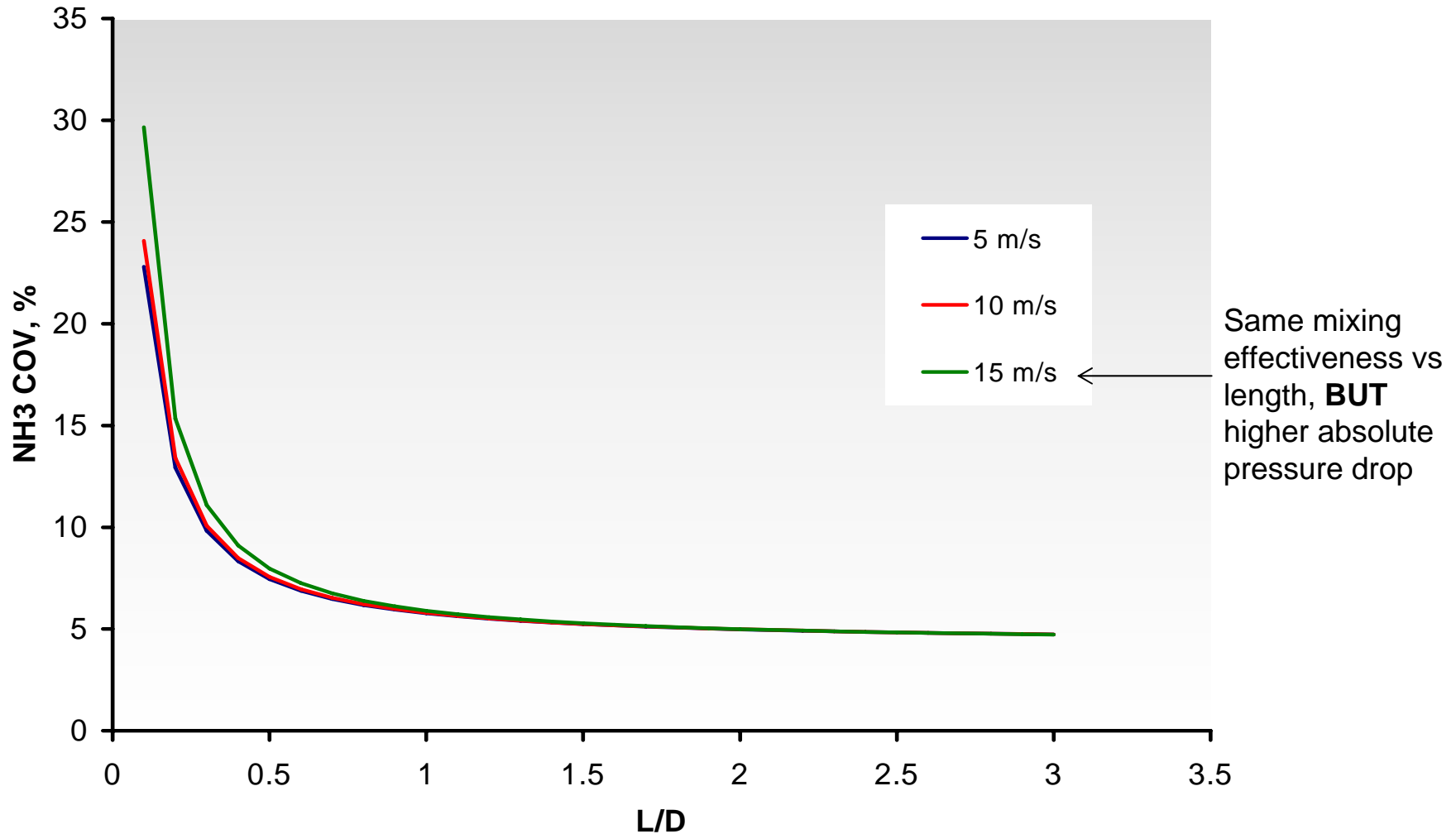


Turbulent Mixing Theory

99% Decay time versus Reynolds Number



Effect of Velocity





Mixing Fundamentals

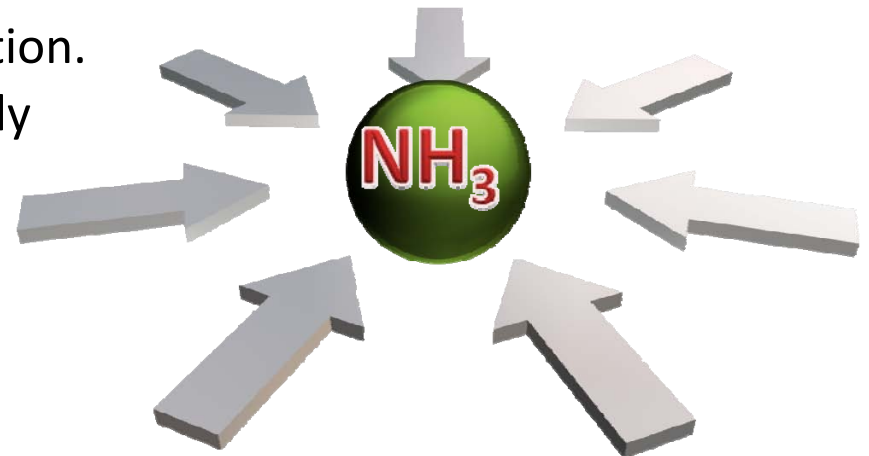
Mixing is dominated by three primary factors

1. Original Distribution – How well a compounds are present or deposited over the space, volume or flowing stream
2. Stretching and Folding – How larger regions of varying concentrations are being divided, thinned and spread across the area via macroscopic turbulence
3. Molecular Diffusion – Occurring simultaneously throughout and necessary for the final an approach to complete homogeneity – influenced & facilitated by the increased surface area brought about by 1 & 2

SCR Ammonia Injection

Important aspects of initial ammonia dosing:

- 1. Flow Dosing** – Matching regional or local ammonia flow to the regional or local flue gas flow (Flow profiles across the AIG are fairly stable across wide load variations – allows stable dosing of ammonia into those flow volumes)
- 2. NO_x Dosing** – Matching of regional or local ammonia flow to the regional or local NO_x concentration (NO_x profiles more apt to change vs load or changing operation. High & low concentration regions can move, or entirely flip in position. Fixed AIG adjustments are thus inherently less stable with respect to NO_x dosing)



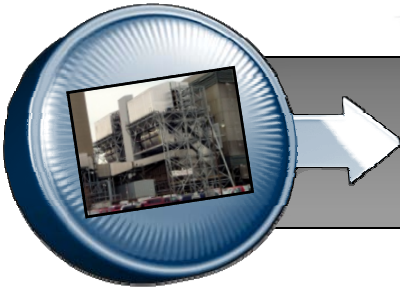
SCR Ammonia Injection

- 3. *Spatial Dosing*** – Spacing of the injection points and thus the injection point quantity:
- ▶ One large blob, a few smaller ones, or more distributed?
 - ▶ Closer spacing improves final blend of the dosed component only. There is a point of diminishing return.
 - ▶ Too many increases flue blockage, pipe routing.
 - ▶ Too sparse can reduce overall system effectiveness and efficiency and can oversensitize placement relative to mixer vane, plate or disc elements.
 - ▶ Optimum number and size is influenced by the design (penetrating vs non-penetrating, evaporative vs non-evaporative, deposition potential, turbulence at nozzle exit, specific mixer design, etc.)



SCR Mixer Designs

- ▶ All utility coal-fired SCR mixing applications are turbulent flow applications across the entire load range.
- ▶ Many designs have shared performance characteristics.
- ▶ With only some minor exceptions, all designs operating in utility SCR applications today;
 1. Maintain a relatively constant blend across all load ranges.
 2. Will experience a deterioration in the final blend entering the catalyst bed as NO_x distributions deteriorate leaving the boiler.



SCR Mixer Designs

Vortex mixers

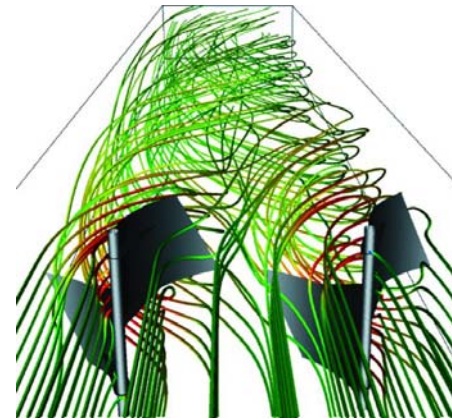
- ▶ Blend largely from downstream vortices
- ▶ A small portion of effectiveness attributable to lateral displacement of flow volumes by the upstream face of the device
- ▶ Typically lower length efficiencies. The larger the vortex, the longer the downstream distance required to fully utilize its mixing potential

Vane mixers

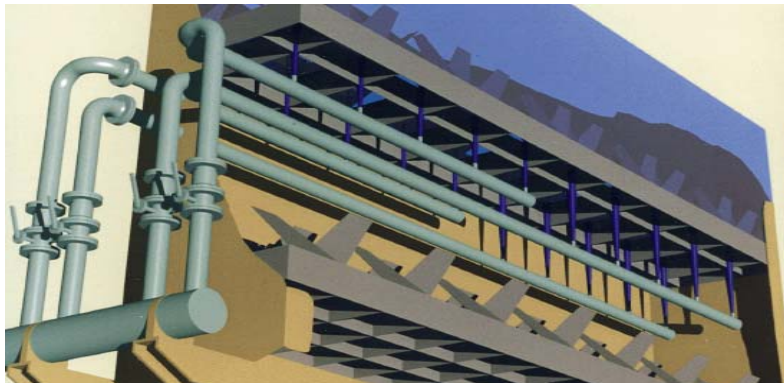
- ▶ Seek to re-direct, laterally displace, divide and recombine flow volumes
- ▶ Translocation of flow volumes is a major source of effectiveness
- ▶ In turbulent applications, vortices internal and downstream produced by exiting dissimilar flow trajectories, contribute to effectiveness
- ▶ Can have improved length efficiency over vortex. (Mixing effectiveness may also wash out in shorter distance)

Hybrid mixers seek to exploit the benefits of each basic concept

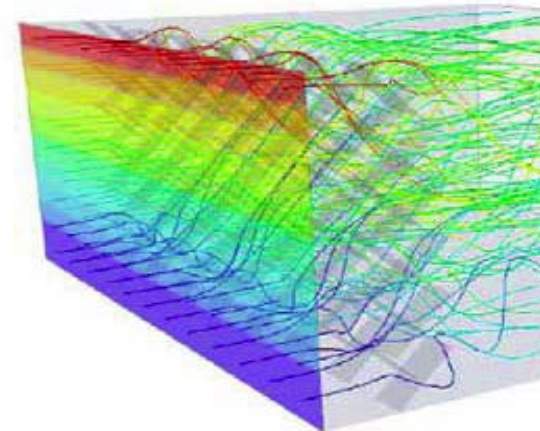
Mixer Designs and Options Vary



Sulzer Chemtech – Vane and Vortex/Hybrid

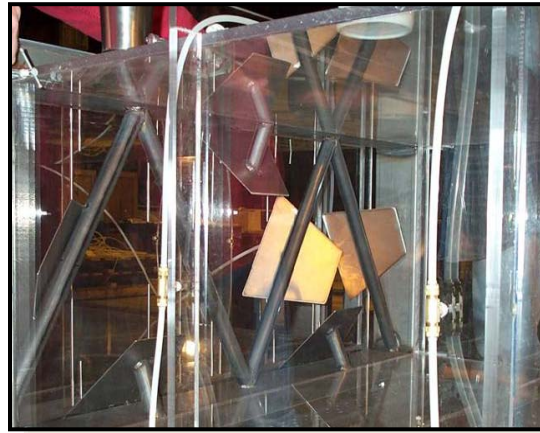
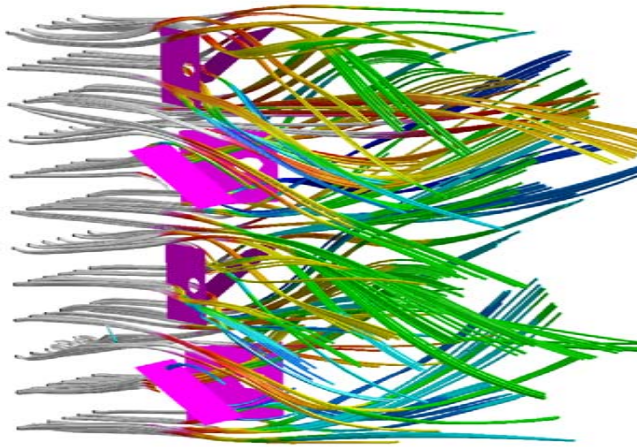


(Parmix & Turbomix – Vane/Hybrid)



Fuel Tech – Vane/Hybrid

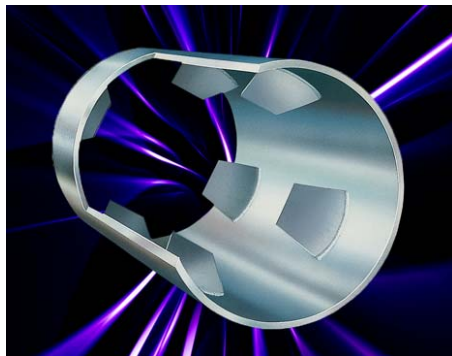
Mixer Designs and Options Vary



Babcock & Wilcox – Vane/Hybrid & Vortex/Hybrid



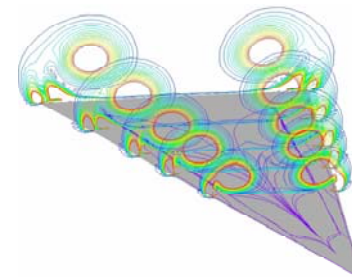
SPX Balcke-Durr
(Delta Wing) Vortex



Vortex
Others

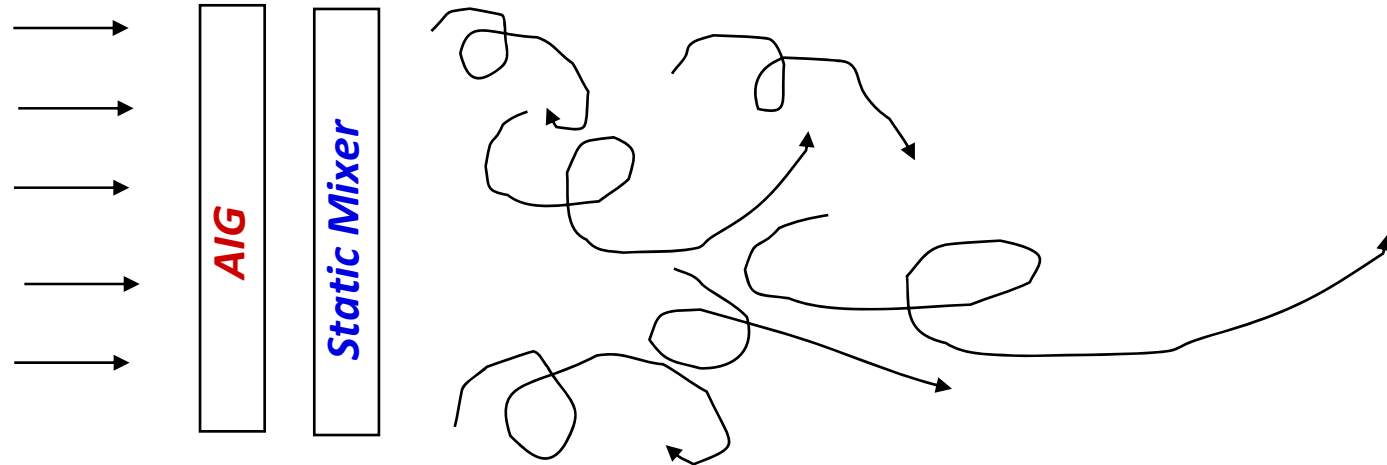


Vane/Hybrid

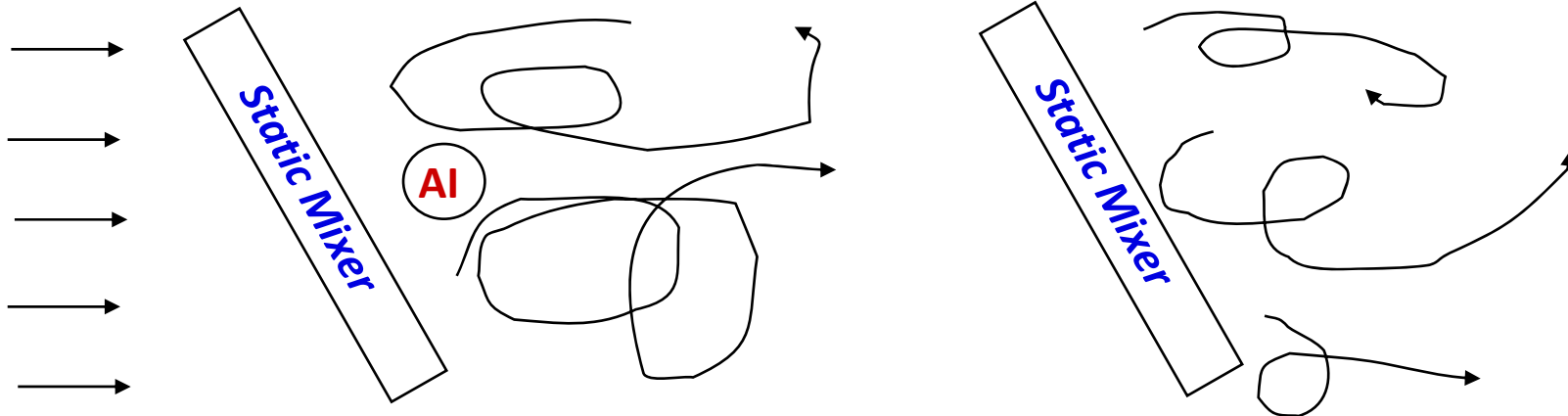


Classical Delta
Wing

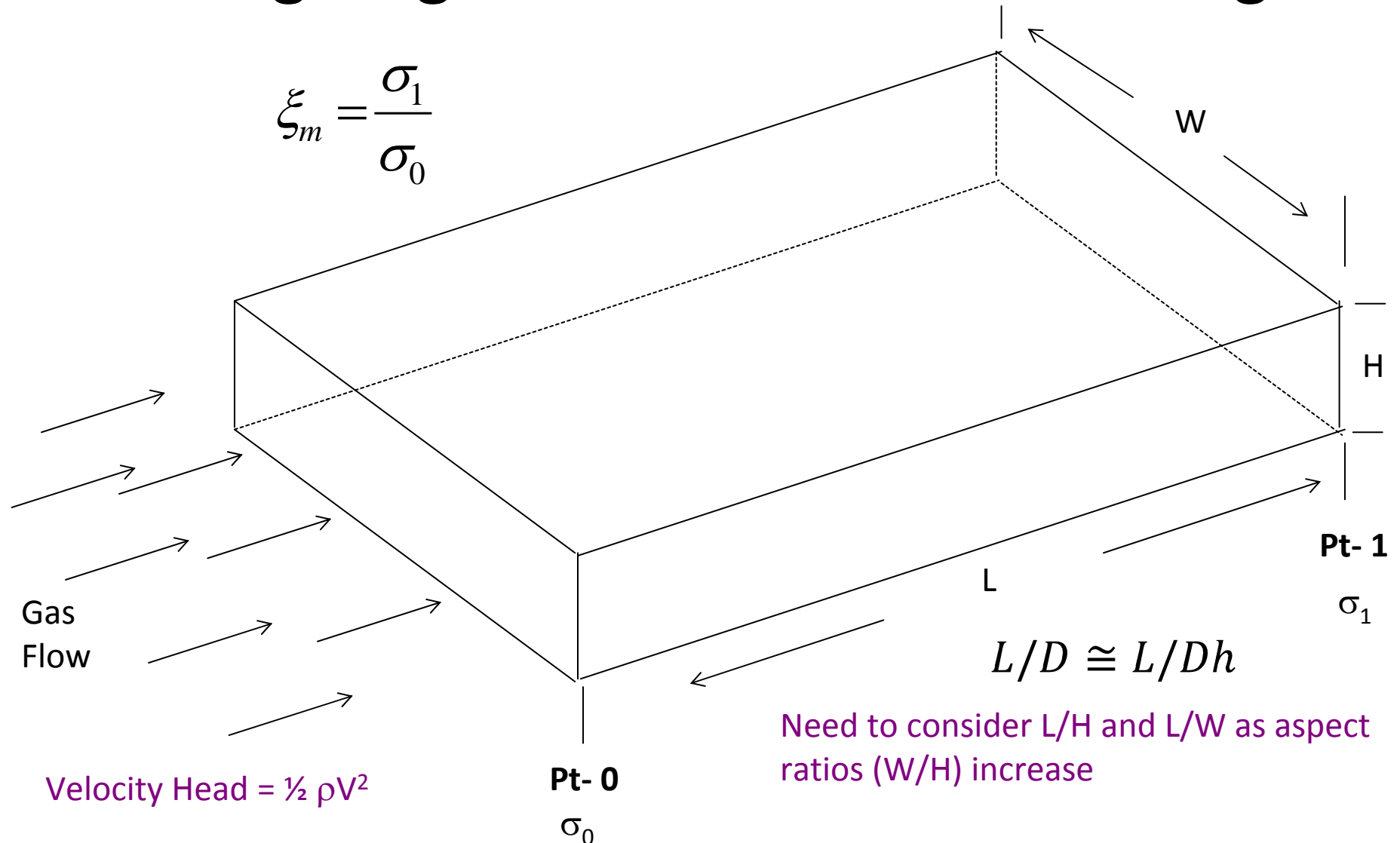
Ammonia Injection & Mixing Approach



Increasing Duct Length



Designing for Whole Duct Blending



Need to consider L/H and L/W as aspect ratios (W/H) increase

Mixing Effectiveness versus Efficiency

Mixing Effectiveness Parameter

$$\xi_m' = 1 - \frac{\sigma_1}{\sigma_0}$$

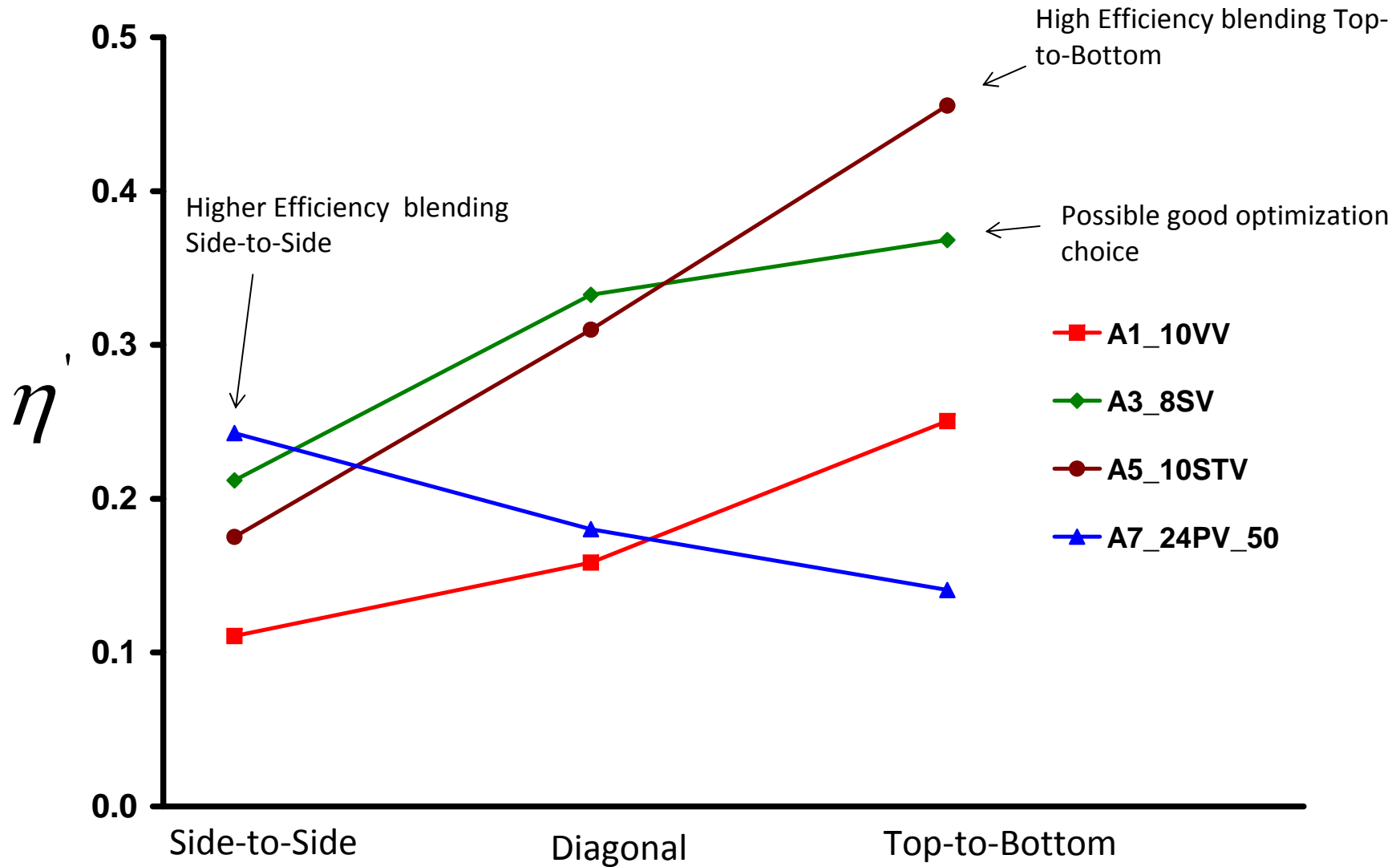
Mixer Shock Loss Coefficient

$$\zeta_m = \frac{\Delta P_m}{\rho V^2 / 2}$$

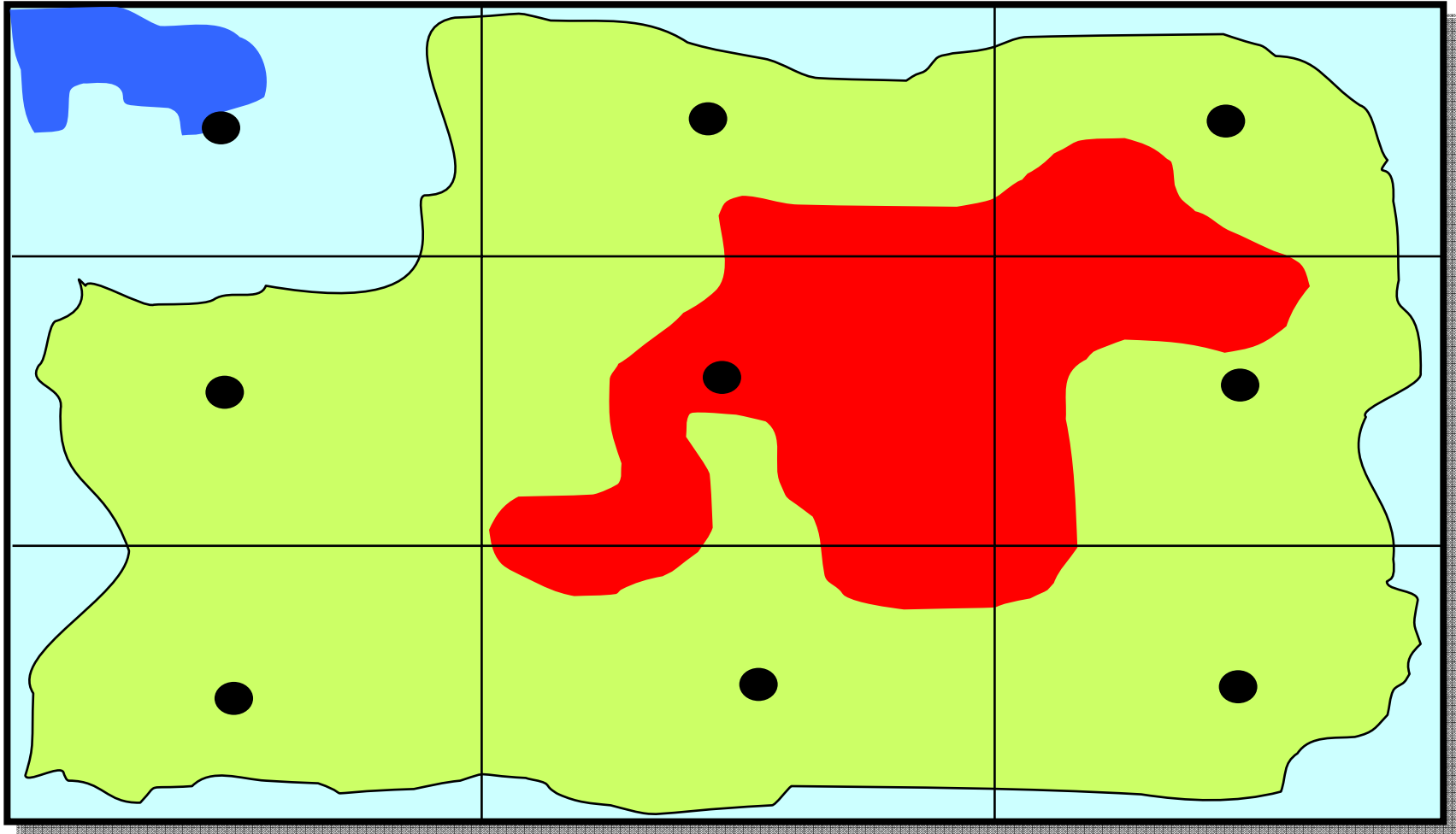
Dimensionless Mixing Efficiency

$$\eta_m' = \frac{\xi_m'}{\zeta_m}$$

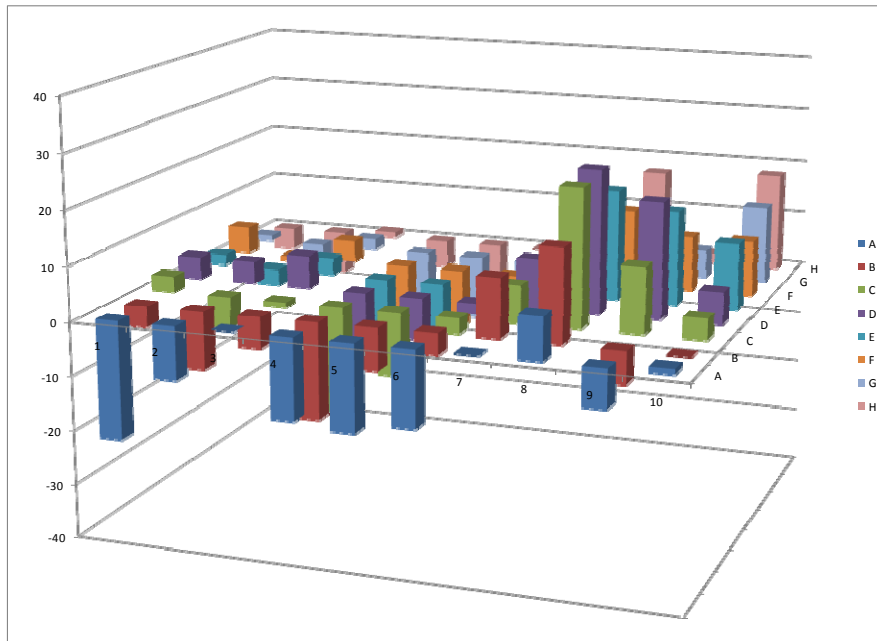
Mixer Efficiency & Directivity



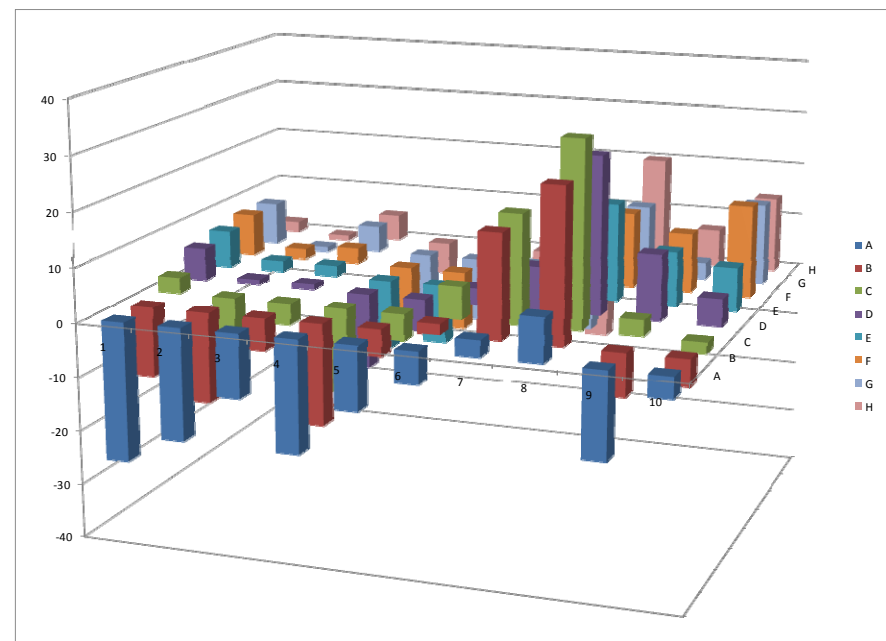
AIG Dosing



Velocity Variation at AIG versus Load

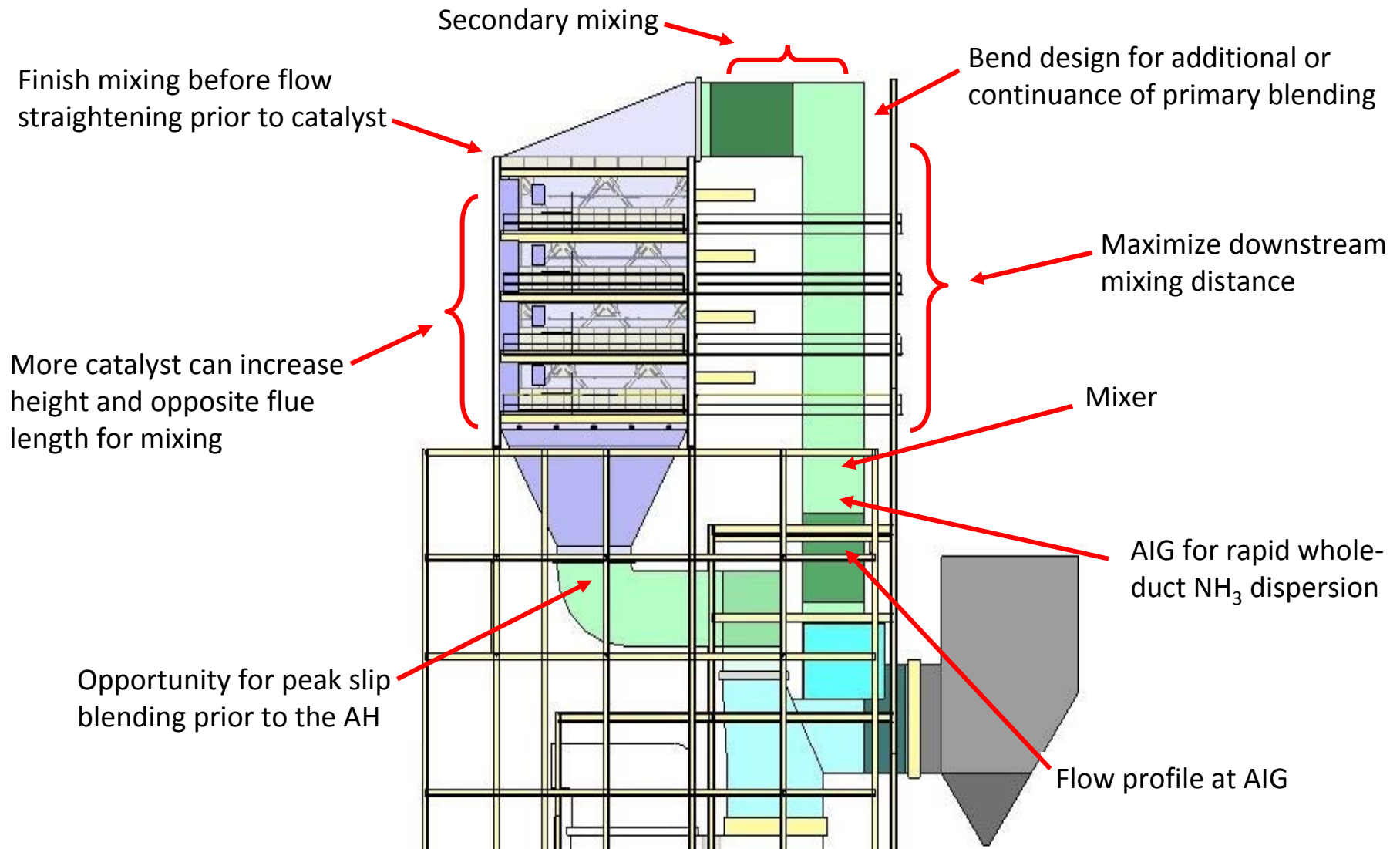


100% Load



40% Load

Arrangements for Promotion of Mixing



Actual Field Uniformity Performance

Field Site →	A	B	C	D	E
Mixer Design	Other	Other	B&W	B&W	B&W
Removal Efficiency, %	87%	86%	92%	93%	89%
SCR Outlet NOx COV	18%	23%	16%	10%	24%
SCR Inlet NH3/NOx COV	2.5%	3.8%	1.9%	1.2%	3.2%
Relative Mix Length	1.5	3.3	1.0	2.7	2.8
Relative Shock Loss	2.0	1.0	2.7	3.3	1.3

Summary

Multiple approaches exist for SCR -

- ▶ Appear to be functioning adequately (Some better than expected)
- ▶ Only a few reports of plugging (Injection point eddies, support build-up)
- ▶ Ammonia injection before primary mixing elements.
- ▶ Ammonia injection after primary mixing elements.

Important optimization parameters -

- ▶ Initial dosing (AIG design, NO_x profile, flow profile)
- ▶ Injection nozzle quantity and size (Influenced by location and mixer design)
- ▶ Mixer directivity of mixing – low aspect ratio versus high aspect ratio
- ▶ Mixer length efficiency versus energy efficiency
- ▶ Arrangement design (Flue size, dampers, expansions, contractions, bends, hoods, by-pass, etc.)
- ▶ Specified flow velocity uniformity requirements (Not always compatible with best design)

Summary

Field performance is tracking predicted well

- ▶ Effectiveness is being proven and efficiencies are being established
- ▶ Verifying non-plugging AIG designs are indeed non-plugging
- ▶ Fundamentals remain applicable and are being validated
- ▶ Some approaches can become impractical as L/D drops
- ▶ Process result limitations can occur at very low L/D
- ▶ Turbulent mixer characteristics apply to all turbulent mixers
- ▶ Designing for **'Set it and forget it'** tuning
- ▶ Avoid over tuning!
- ▶ AIG flow profile verification (review model study or traverse of actual)
- ▶ Goal is to deliver the best, most stable blend, at the lowest possible energy consumption within a given arrangement
- ▶ Research for improved configurations is continuing in support of increasingly stringent demands (high process result and/or poor arrangement)

B&W

power generation group

THANK YOU!

Kevin Rogers
Advisory Engineer
